

# General Equation to Determine Design Rules for Mitigating Partial Discharge and Electrical Breakdown in Power Module Layouts

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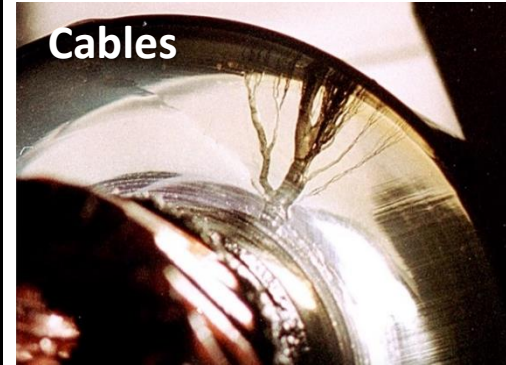
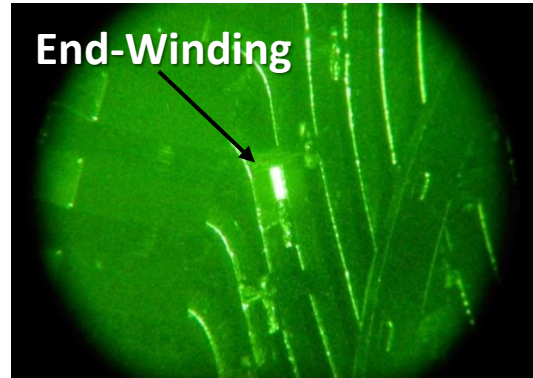
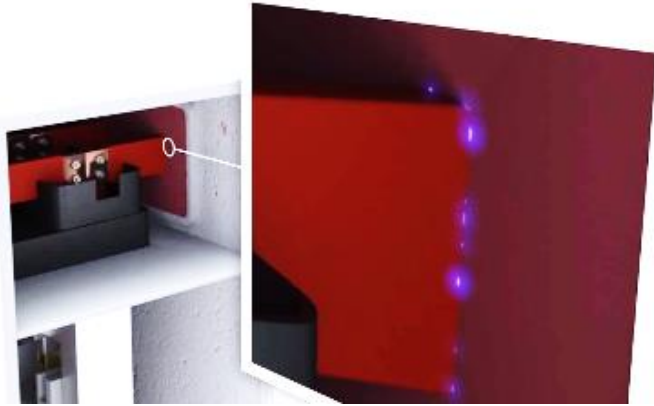
Shilpi Mukherjee, Dr. Yarui Peng, and Dr. Alan Mantooth

University of Arkansas, Fayetteville, USA

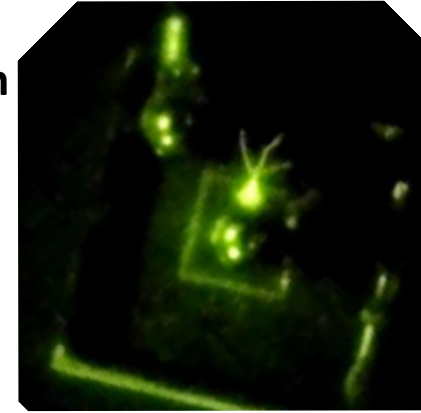
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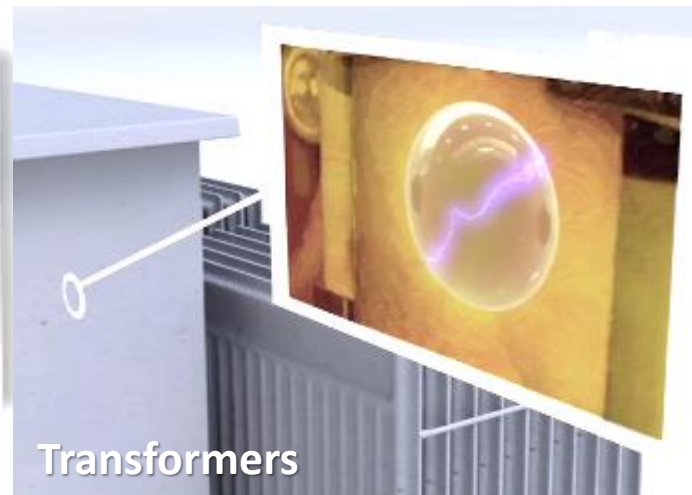
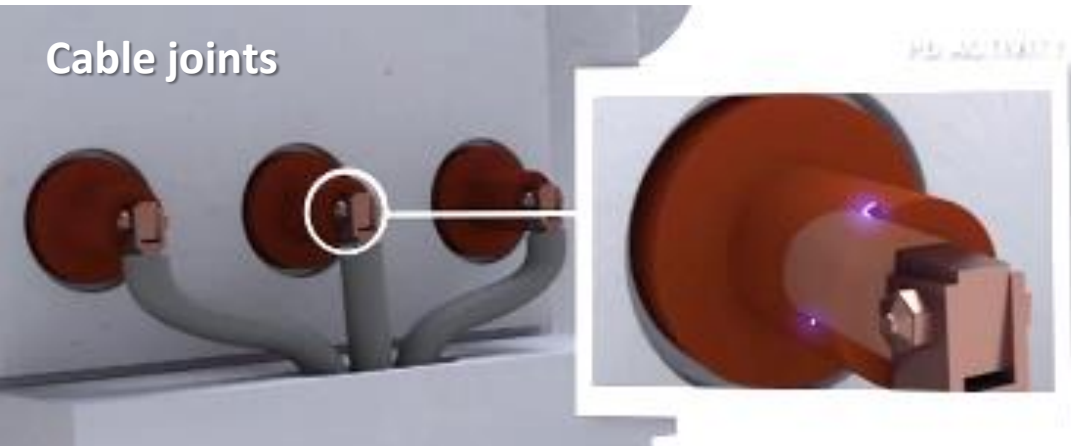
# Partial Discharge



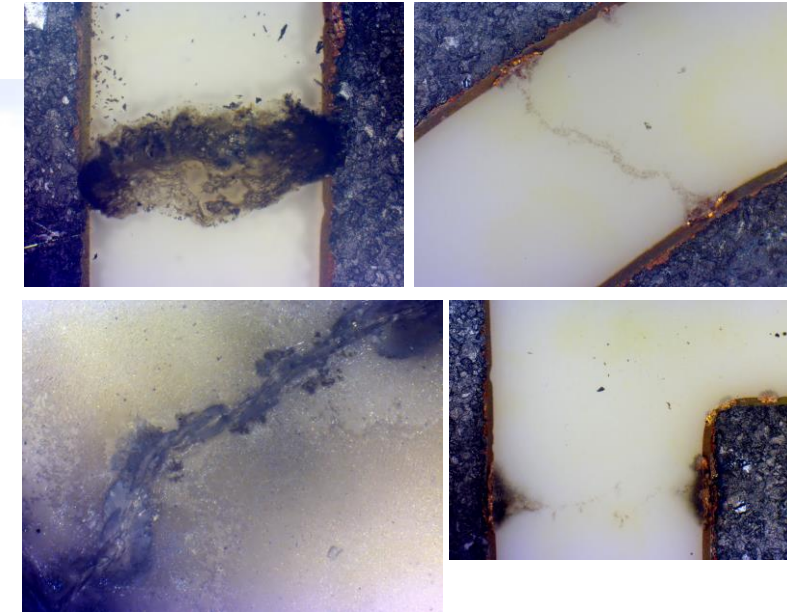
DBC test coupon



Cable joints



Transformers



<https://www.youtube.com/watch?v=QSivGicvtNM>

# Existing PD Models

- ❑ Electrical Point of View

  - Three-capacitor (ABC) model

- ❑ Field Point of View

  - ❑ Pederson's model – considers volume and surface charge density

  - ❑ Conductance model – considers current density

  - ❑ Niemeyer's model – considers avalanche and streamer propagation

  - ❑ Plasma model – fluid equations

  - ❑ Numerical simulation model – temporal and spatial distribution

- ❑ Other models

Partial Discharge

Existing Models

2D Simulations

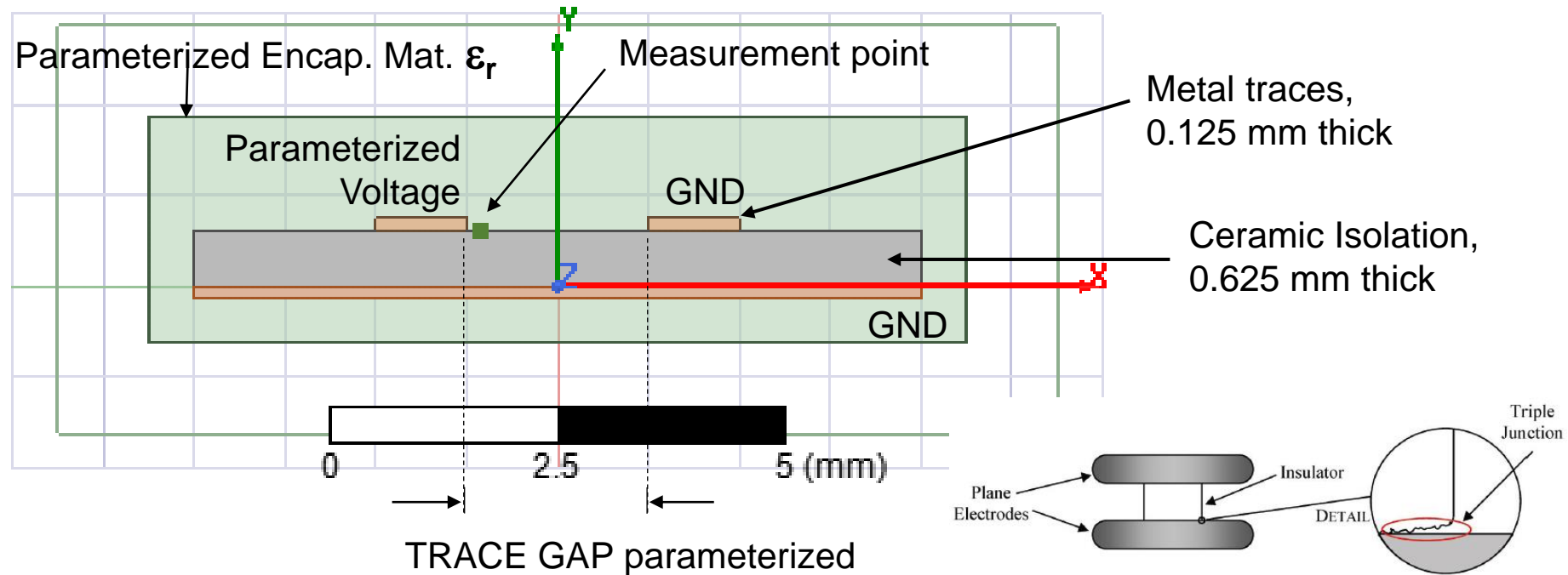
3D Simulations

Design Rule  
Implementation in  
PowerSynth

Effect of Filletting

# 2D Simulations

## Model geometry



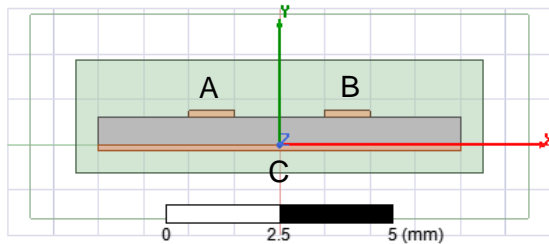
Parameter range:

Trace gap: 0.5mm to 5.0mm     $\epsilon_r$  : 1 to 10    Voltage: 5kV to 30kV

- Partial Discharge
- Existing Models
- 2D Simulations
- 3D Simulations
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# 2D Simulations

## Model geometry



## Parameter range:

Trace gap: 0.5mm to 5.0mm  
step size: 0.5mm

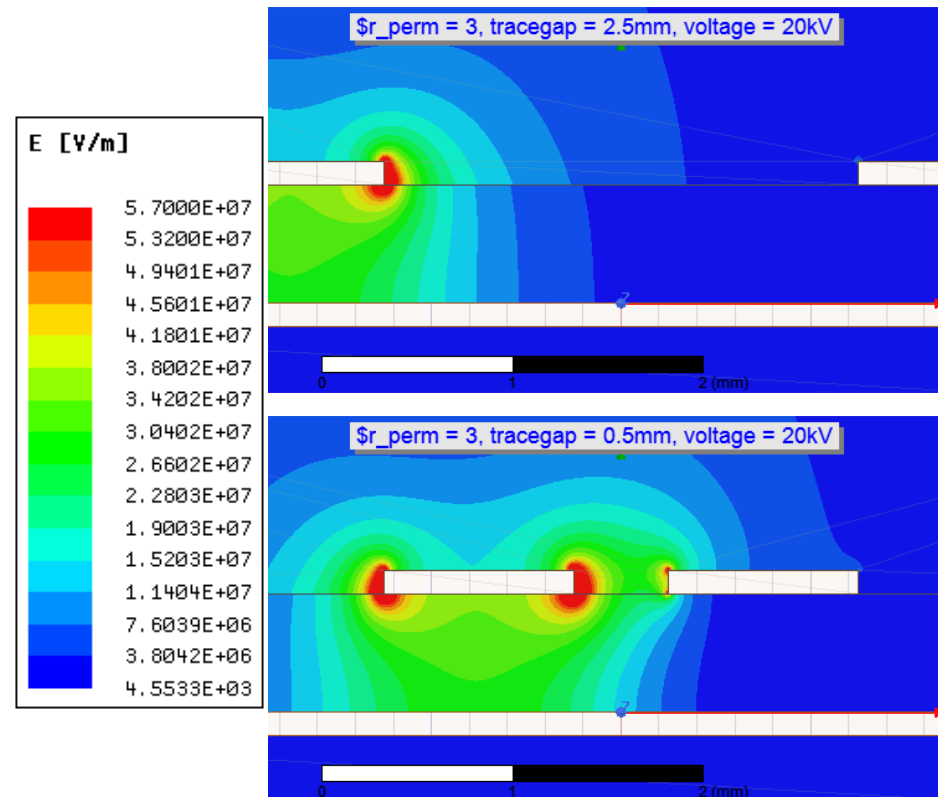
$\epsilon_r$  : 1 to 10

step size: 1

Voltage: 5kV to 30kV

step size: 5kV

## E-field distribution



Partial Discharge

Existing Models

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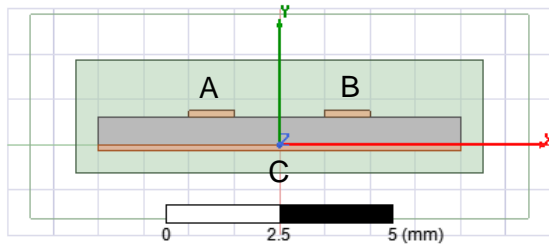
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# 2D Simulations

## Model geometry



## Parameter range:

Trace gap: 0.5mm to 5.0mm  
step size: 0.5mm

$\epsilon_r$  : 1 to 10

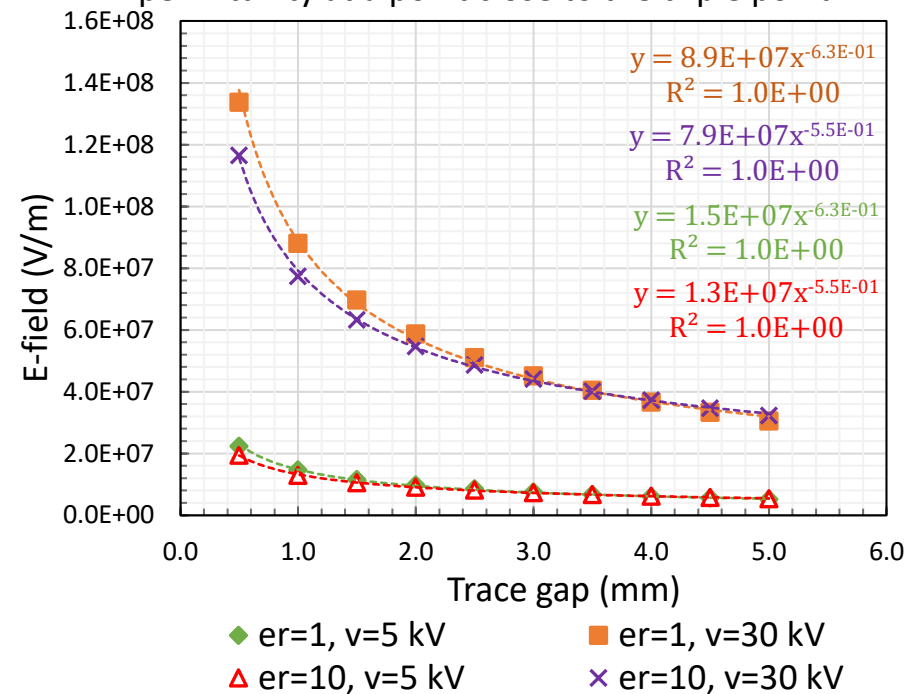
step size: 1

Voltage: 5kV to 30kV

step size: 5kV

## Power curves

E-field vs. trace gap for corner cases of the parametric sweep of voltage and relative permittivity at a point close to the triple point



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# 2D Simulations

## General form of equation

$$E = f(v, \epsilon_r) x^{-g(v, \epsilon_r)}$$

Where

$E$  is the electric field in kV/mm,

$v$  is the voltage in kV,

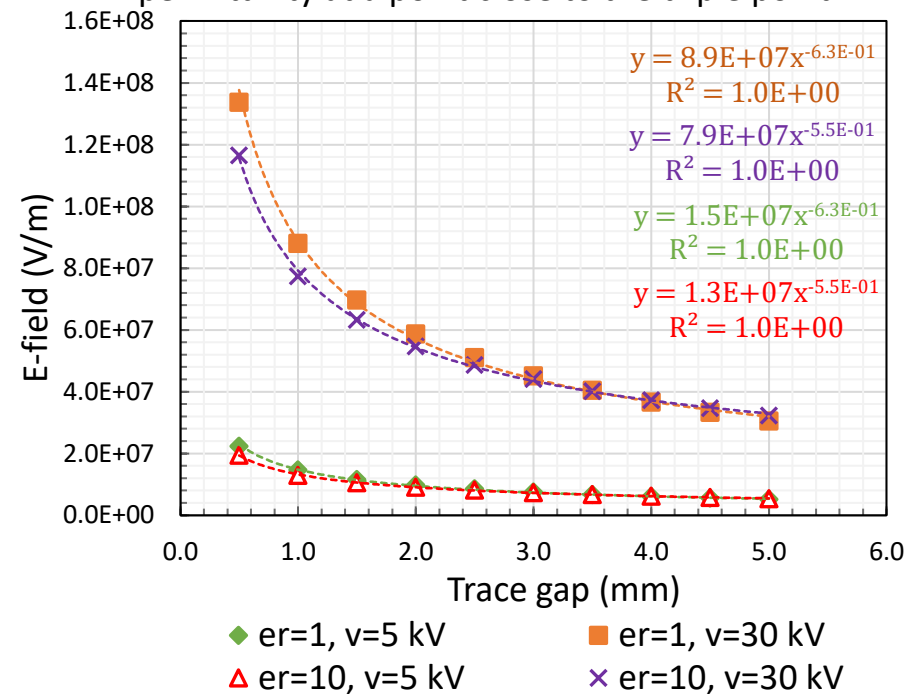
$x$  is the gap between traces A and B in mm,

$\epsilon_r$  is the relative permittivity of the encapsulating material

$f$  and  $g$  are functions of  $v$  and  $\epsilon_r$ .

## Power curves

E-field vs. trace gap for corner cases of the parametric sweep of voltage and relative permittivity at a point close to the triple point



Partial Discharge

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# 2D Simulations

General form of equation

$$E = \frac{v}{5} f_{5kV}(\epsilon_r) x^{-g(v, \epsilon_r)}$$

Where

$E$  is the electric field in kV/mm,

$v$  is the voltage in kV,

$x$  is the gap between traces A and B in mm,

$\epsilon_r$  is the relative permittivity of the encapsulating material

$f$  and  $g$  are functions of ( $v$  and)  $\epsilon_r$ .

Coefficient,  $\frac{v}{5} f_{5kV}(\epsilon_r)$  in mC/m<sup>2</sup>

| $\epsilon_r$ | 5 kV | 10 kV | 15 kV | 20 kV | 25 kV | 30 kV |
|--------------|------|-------|-------|-------|-------|-------|
| 1            | 1.48 | 2.96  | 4.43  | 5.91  | 7.75  | 8.87  |
| 2            | 1.48 | 3.02  | 4.27  | 5.75  | 7.60  | 9.11  |
| 3            | 1.41 | 2.94  | 4.23  | 5.61  | 7.51  | 9.11  |
| 4            | 1.38 | 2.77  | 4.15  | 5.74  | 7.17  | 8.30  |
| 5            | 1.62 | 2.90  | 4.24  | 5.48  | 7.22  | 8.64  |
| 6            | 1.39 | 2.78  | 4.07  | 5.51  | 6.88  | 8.18  |
| 7            | 1.35 | 2.69  | 4.03  | 5.38  | 6.80  | 8.20  |
| 8            | 1.35 | 2.72  | 4.05  | 5.41  | 6.80  | 8.11  |
| 9            | 1.33 | 2.67  | 4.00  | 5.35  | 6.66  | 8.01  |
| 10           | 1.32 | 2.64  | 3.96  | 5.29  | 6.61  | 7.92  |

Exponent,  $g(v, \epsilon_r)$

| $\epsilon_r$ | 5 kV | 10 kV | 15 kV | 20 kV | 25 kV | 30 kV |
|--------------|------|-------|-------|-------|-------|-------|
| 1            | 0.63 | 0.63  | 0.63  | 0.63  | 0.66  | 0.63  |
| 2            | 0.56 | 0.55  | 0.51  | 0.55  | 0.53  | 0.53  |
| 3            | 0.57 | 0.54  | 0.49  | 0.51  | 0.57  | 0.53  |
| 4            | 0.56 | 0.56  | 0.51  | 0.60  | 0.56  | 0.51  |
| 5            | 0.53 | 0.61  | 0.56  | 0.54  | 0.56  | 0.55  |
| 6            | 0.54 | 0.53  | 0.54  | 0.55  | 0.53  | 0.56  |
| 7            | 0.52 | 0.53  | 0.53  | 0.53  | 0.54  | 0.54  |
| 8            | 0.54 | 0.54  | 0.54  | 0.55  | 0.56  | 0.56  |
| 9            | 0.55 | 0.55  | 0.55  | 0.55  | 0.55  | 0.54  |
| 10           | 0.55 | 0.55  | 0.55  | 0.55  | 0.55  | 0.55  |

Partial Discharge

Existing Models

2D Simulations

3D Simulations

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# 3D Simulations

## General form of equation

$$Q_s = f(v, \epsilon_r) x'^{-g(v, \epsilon_r)}$$

$$\rightarrow Q_s = \frac{v}{2.5} f(\epsilon'_r) x'^{-g(\epsilon'_r)}$$

Where

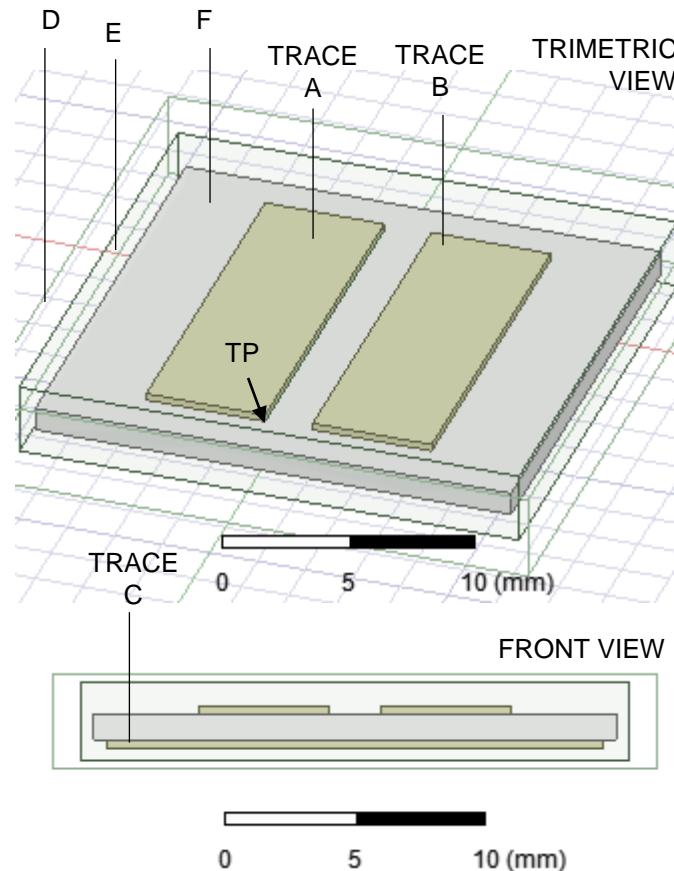
$Q_s$  is the surface charge density in  $\text{mC}/\text{m}^2$ ,  
 $v$  is the voltage in kV,

$x'$  is the ratio of the gap between traces A and B, and the gap between traces A and C.

$\epsilon'_r$  is the relative permittivity of the encapsulating material relative to the relative permittivity of the ceramic,

$f$  and  $g$  are functions of  $\epsilon'_r$ .

## Model geometry



- A: Variable voltage Cu trace
- B: 0 V Cu trace
- C: 0 V back side Cu trace
- D: Balloon boundary region
- E: Encapsulant material
- F: Ceramic ( $\text{Al}_2\text{O}_3$ )
- TP: Triple point
- MP: Measurement point
- Ceramic thickness: 1mm
- Metal thickness: 0.3mm

Partial Discharge

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2D Simulations

**3D Simulations**

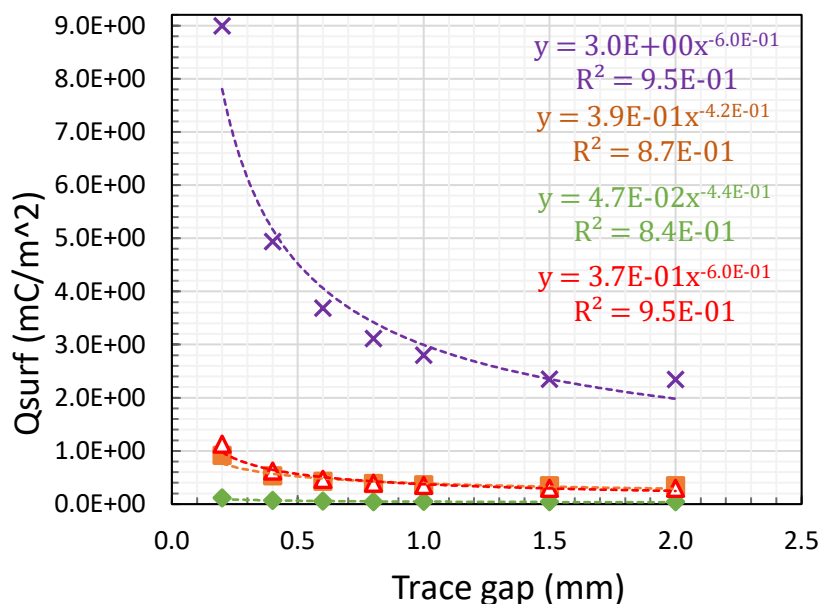
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# 3D Simulations

## Power curves

Surface charge density vs. trace gap for corner cases of the parametric sweep of voltage and relative permittivity



◆ er Ratio=0.1, v=2.5 kV    ■ er Ratio=0.1, v=20 kV  
 ▲ er Ratio=1.0, v=2.5 kV    ✕ er Ratio=1.0, v=20 kV

Coefficient,  $[v/2.5 f(\epsilon'_r)]$  in mC/m<sup>2</sup>

| $\epsilon_r$ | $\epsilon'_r$ | 2.5 kV | 5 kV  | 7.5 kV | 10 kV | 15 kV | 20 kV |
|--------------|---------------|--------|-------|--------|-------|-------|-------|
| 1            | <b>0.102</b>  | 0.047  | 0.097 | 0.150  | 0.190 | 0.290 | 0.390 |
| 2            | <b>0.204</b>  | 0.093  | 0.190 | 0.280  | 0.370 | 0.560 | 0.740 |
| 3            | <b>0.306</b>  | 0.130  | 0.270 | 0.400  | 0.530 | 0.800 | 1.100 |
| 4            | <b>0.408</b>  | 0.170  | 0.340 | 0.520  | 0.690 | 1.000 | 1.400 |
| 7            | <b>0.714</b>  | 0.280  | 0.550 | 0.830  | 1.100 | 1.700 | 2.200 |
| 10           | <b>1.020</b>  | 0.370  | 0.750 | 1.100  | 1.500 | 2.200 | 3.000 |

$$f = 0.35\epsilon'_r + 0.02$$

Exponent,  $g(\epsilon'_r)$

| $\epsilon_r$ | $\epsilon'_r$ | All voltages |
|--------------|---------------|--------------|
| 1            | <b>0.102</b>  | 0.42         |
| 2            | <b>0.204</b>  | 0.45         |
| 3            | <b>0.306</b>  | 0.48         |
| 4            | <b>0.408</b>  | 0.50         |
| 7            | <b>0.714</b>  | 0.56         |
| 10           | <b>1.020</b>  | 0.60         |

$$g = 0.20\epsilon'_r + 0.40$$

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**3D Simulations**

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# 3D Simulations

## General form of equation

$$Q_s = \frac{v}{2.5} f(\epsilon'_r) x^{-g(\epsilon'_r)}$$

$$\rightarrow x = e^{\left(\frac{1}{g} \ln\left(\frac{v}{2.5} f(\epsilon'_r) \frac{1}{Q_s}\right)\right)}$$

$$\rightarrow x = e^{\left(\frac{1}{g} \ln\left(\frac{v}{2.5} f(\epsilon'_r) \frac{1}{\epsilon_0 \epsilon_r E * 10^9}\right)\right)}$$

$$\rightarrow x = e^{\left(\frac{1}{0.20 \epsilon'_r + 0.40} \ln\left(\frac{v}{2.5} (0.35 \epsilon'_r + 0.02) \frac{1}{\epsilon_0 \epsilon_r E * 10^9}\right)\right)}$$

where

$Q_s$  is the surface charge density in mC/m<sup>2</sup>,

$E$  is the electric field in kV/mm,

$v$  is the voltage in kV,

$x$  is the ratio of the gap between traces A and B, and the gap between traces A and C. For ceramic thickness = 1mm,  $x$  gives trace-gap A-B in mm.

$\epsilon'_r$  is the relative permittivity of the encapsulating material relative to the relative permittivity of the ceramic,

$f$  and  $g$  are functions of  $\epsilon'_r$ .

Partial Discharge

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2D Simulations

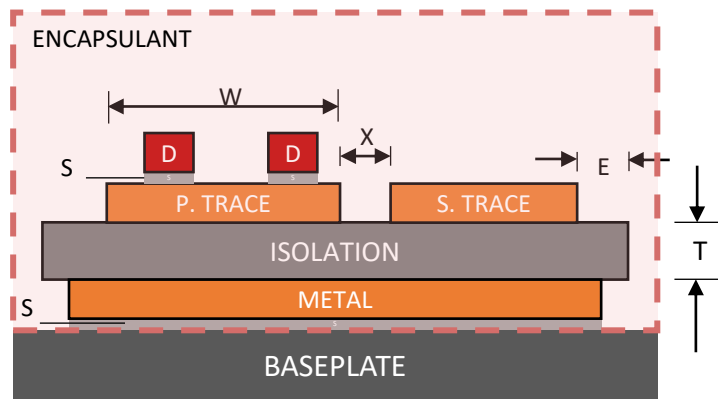
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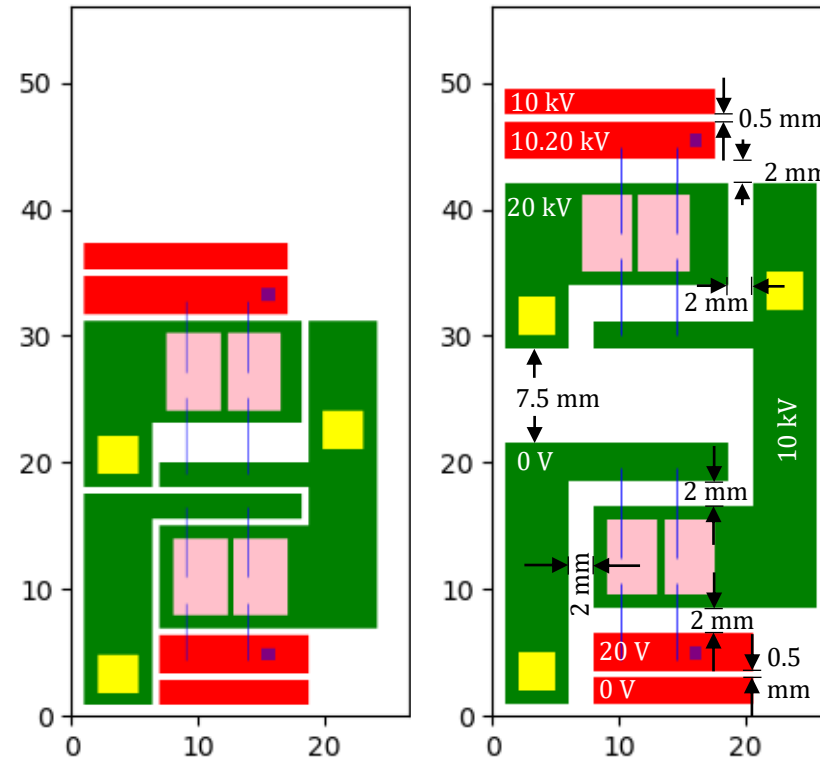
# Implementation in PowerSynth

## Manufacturing Design Kit (MDK) and Design Rule Check (DRC)



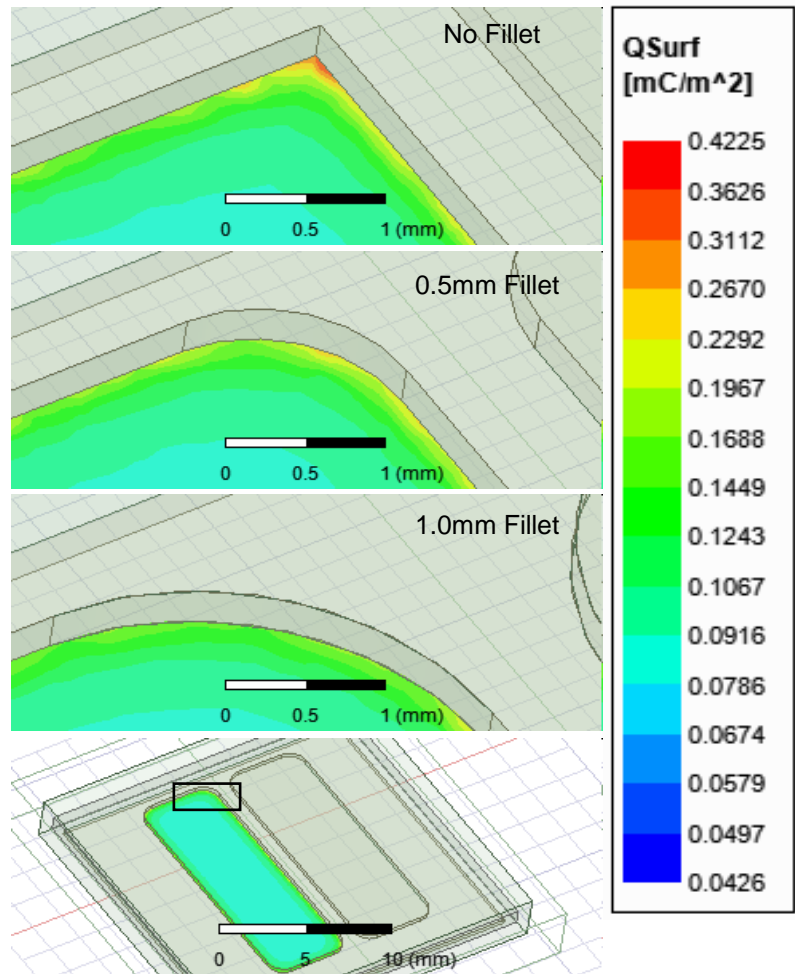
- W: lateral width of trace
- X: lateral trace gap
- E: minimum enclosure
- T: vertical thickness of a layer
- D: device
- P. trace: power trace; S. trace: signal trace
- S: substrate attach or die attach

## Default layout vs. Layout with design rules applied

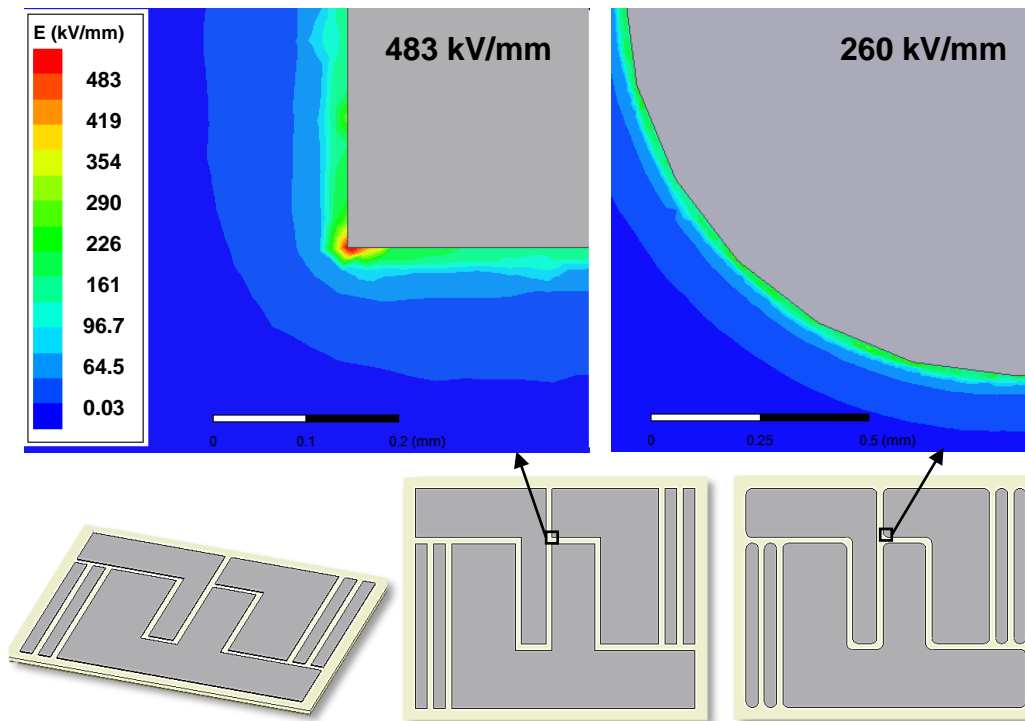


- Partial Discharge
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# Effect of filleting sharp corners



E-field and Q<sub>s</sub> are almost halved



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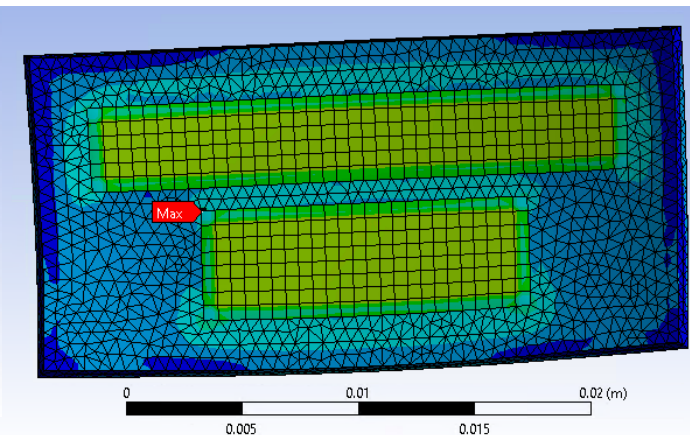
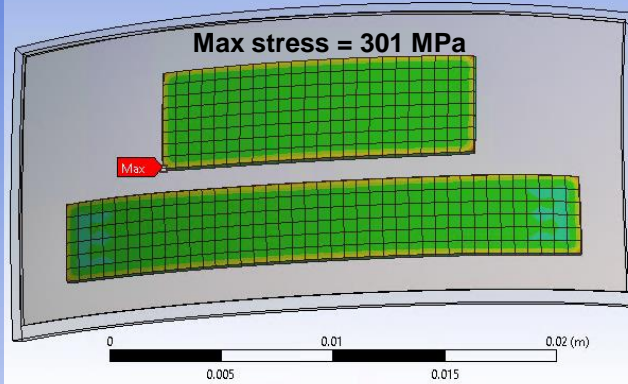
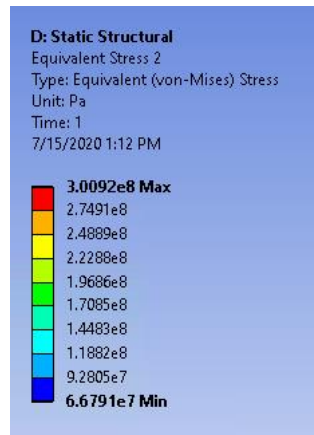
Effect of Filleting

# Filleting reduces mechanical stress

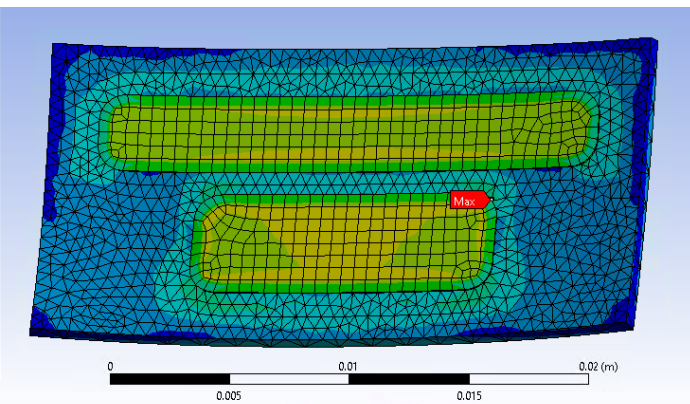
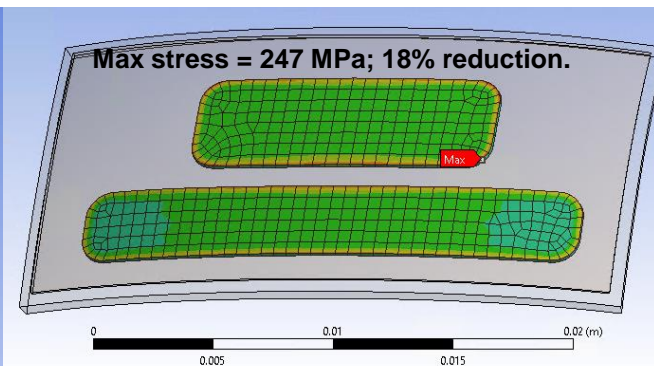
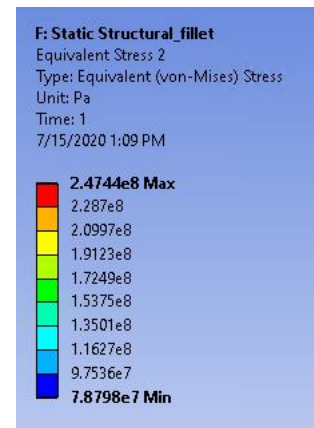
Bottom view

Top view

Sharp



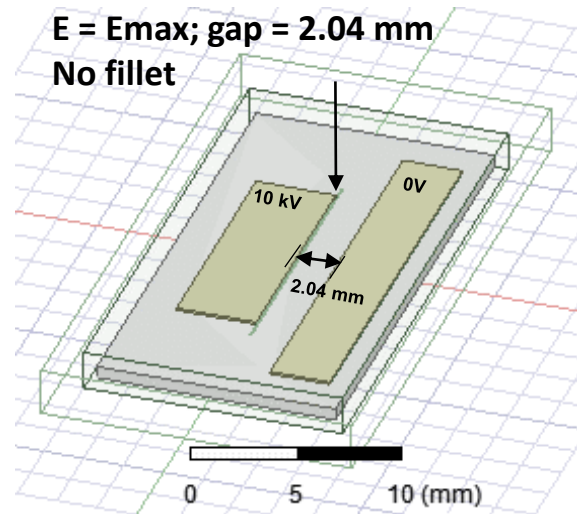
Fillet



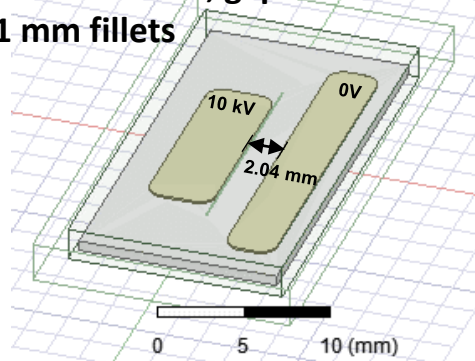
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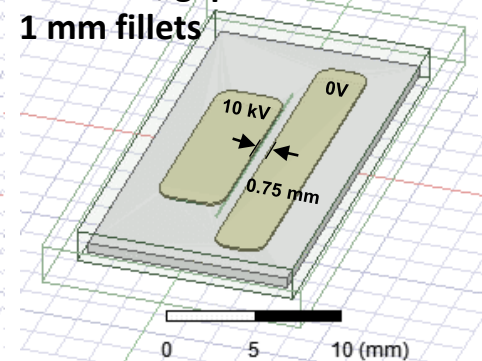
# Effect of filleting sharp corners



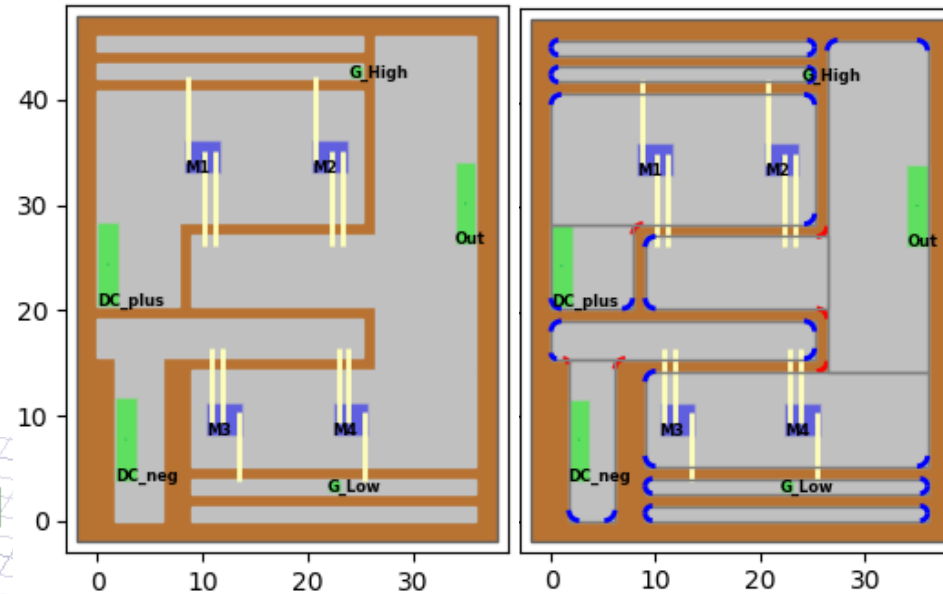
$E = 0.65 E_{max}$ ; gap = 2.04 mm  
1 mm fillets



$E = E_{max}$ ; gap = 0.75 mm  
1 mm fillets



## Application of fillets in PowerSynth



← Gap can be reduced to about 40% of the original gap if fillets are applied.

- Partial Discharge
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# Summary

- ❑ Partial discharge.
- ❑ 2D simulations of E-field focusing.
- ❑ 3D simulations of surface charge density.
- ❑ General equation developed for determining trace gap.
- ❑ Effect of filleting sharp corners.
- ❑ Implementation of trace-gap design rules and fillets in PowerSynth.



# Coming up next...

- ❑ Enhancing the general equation with
  - ❑ Fillet factor,
  - ❑ Derating factor based on wet-etching profile of metal on ceramic,
  - ❑ Derating factor based on voltage profile, and
  - ❑ Metal thickness variation.
- ❑ Statistical analysis through partial discharge tests to determine a margin on design rules because PD is stochastic in nature.

# Acknowledgments

Army Research Lab, USA

and

The National Science Foundation, USA

through P.O.E.T.S (Power Optimization of Electro Thermal Systems)

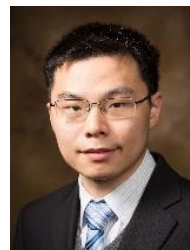
Thanks to WiPDA-Asia for the opportunity to present this research.

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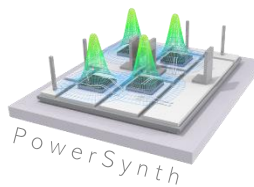
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2020 Japan



P/O/E/T/S



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