



PEEC Method and Hierarchical Approach Towards 3D Multichip Power Module (MCPM) Layout Optimization

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V. Conclusion and future work

- Conclusion and future work
- Acknowledgement



Traditional Module Design Flow

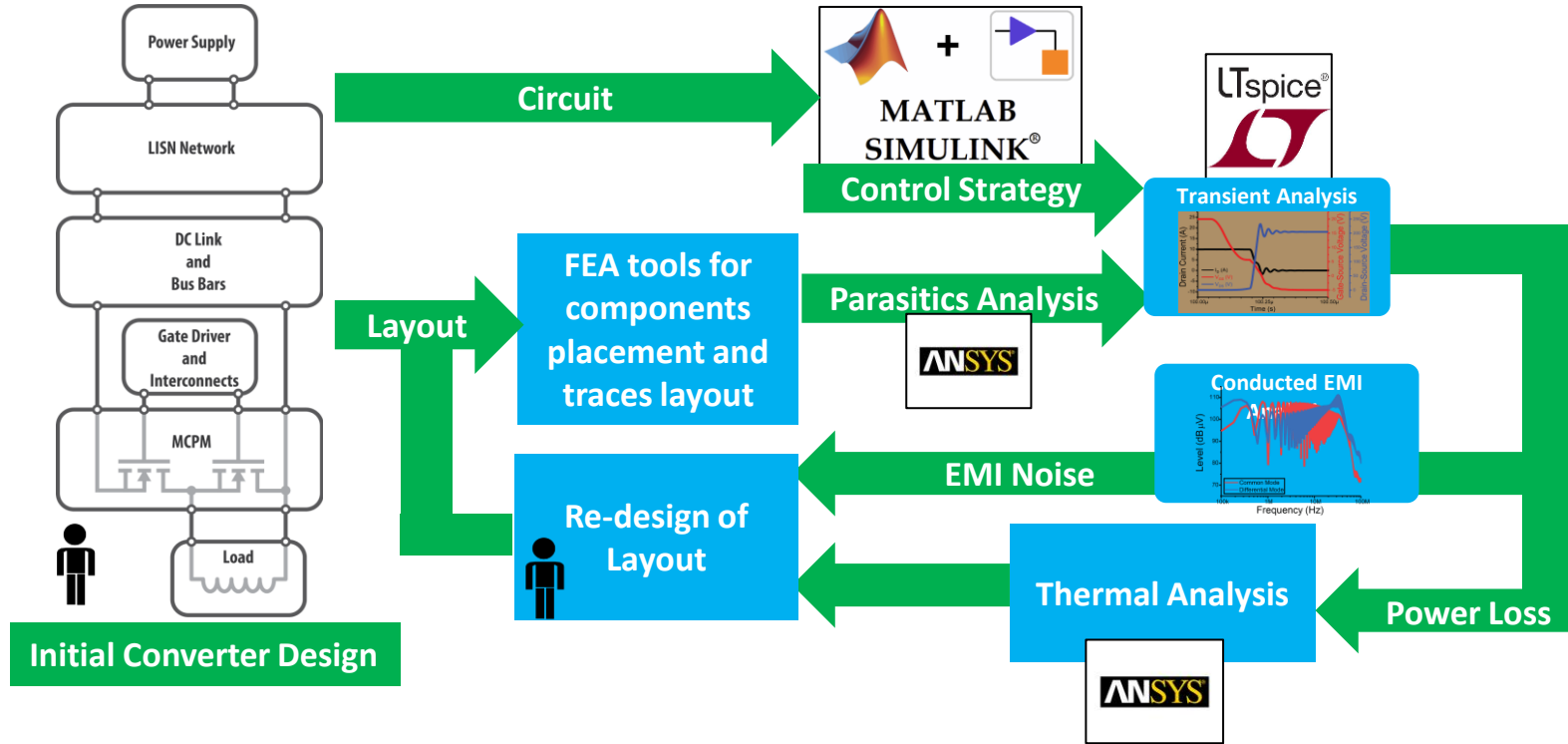
Overview

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The power module design flow is computationally and labor intensive



What Do We Need?

“Imagine we design a circuit without a circuit simulator...
How about designing module layout?”

We need:

- A more efficient design flow.
- Fast and accurate models for electro-thermal assessment.
- An **Electronic Design Automation** tool for Power Module design

**This would enhance the productivity of the
whole design process**

PowerSynth Overview

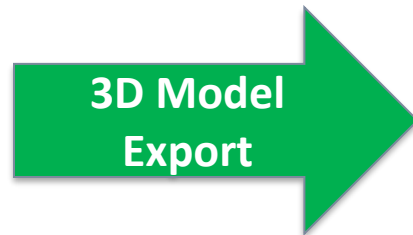
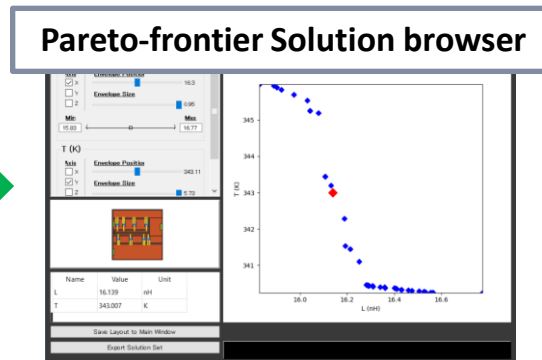
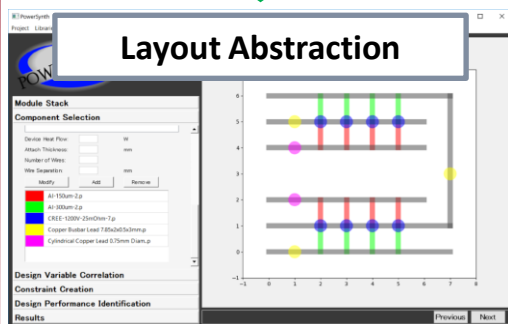
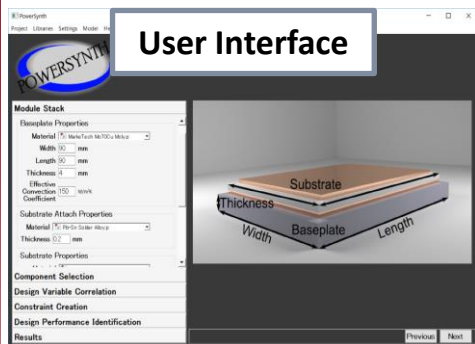
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- **Fast and accurate models**
 - Electrical parasitics
 - Fast 2D thermal model
- **Design automation through multi-objective optimization**
- **Quickly explore trade-offs in solution space**
- **Export to commercial solvers for further analysis**



PowerSynth Design Flow and Strategy

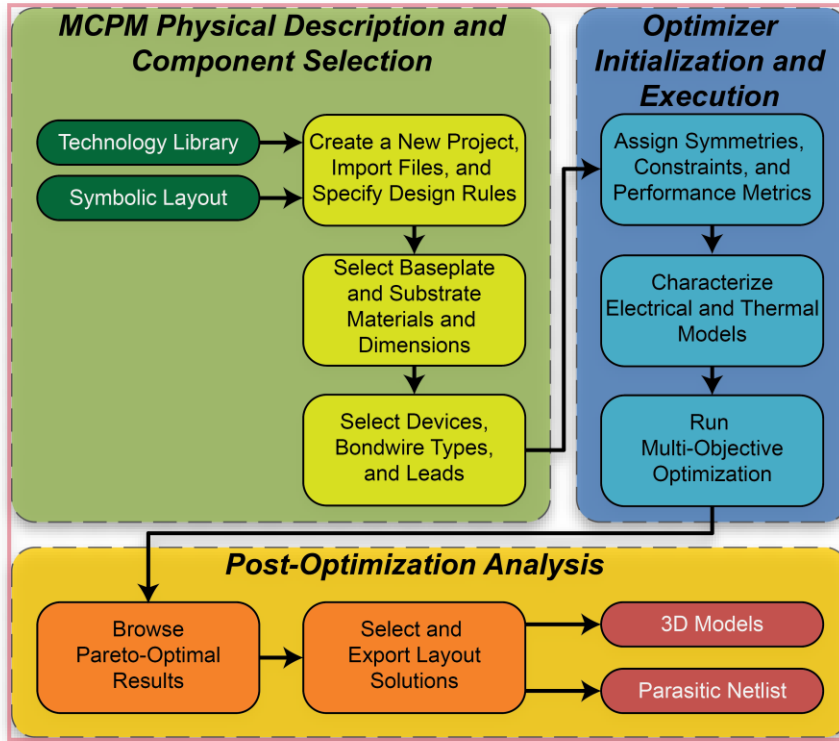
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- Fast layout generation to explore the design spaces of integrated power modules
- Fast thermal and electrical analysis to gauge power module performance quickly
- Multi-objective optimization accounts for many trade-off design solutions.
- Easily export layout solution to FEA tools for post-analysis
- PowerSynth Journal Article [1]



Parasitics Extraction in PowerSynth

Overview

Motivation

Methodology

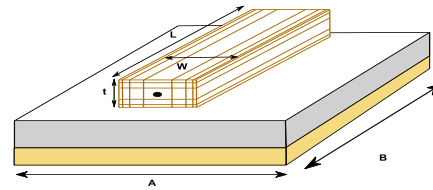
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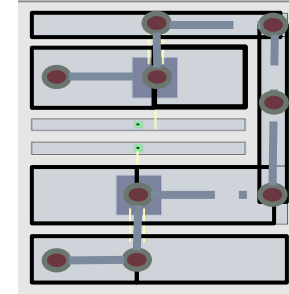
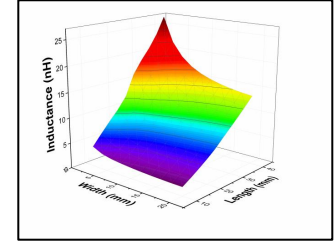
Initial Approach

- **The Laplacian Matrix Method:**
 - Linear approximation of loop Inductance and Resistance values.
 - Fast evaluation and accurate extraction for most 2D layouts
 - Response surface for accurate extraction
- **Limitations:**
 - Does not consider mutual inductance between nets.
 - No branch current and node voltage information

Simulation in FastHenry



Response Surface Model

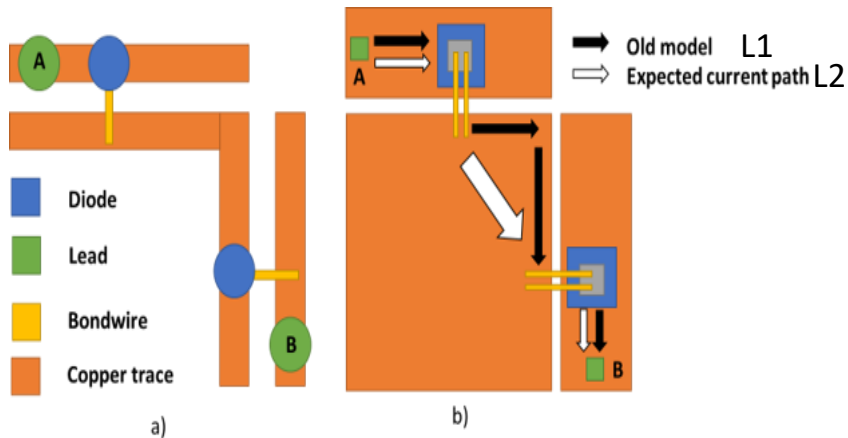


- Connection Nodes
- Rectangular Splits
- Current Path

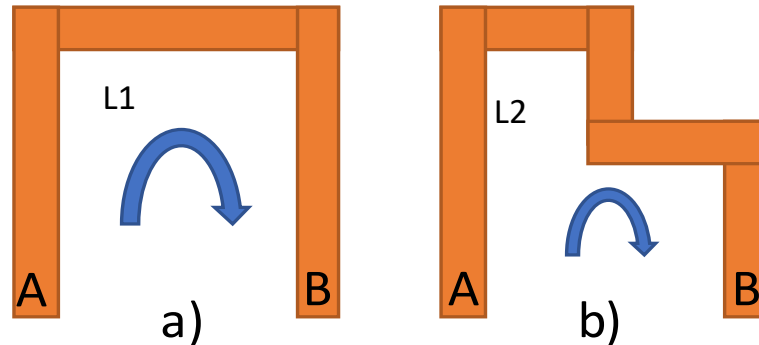
Loop Parasitics Extraction Using Laplacian Matrix

Limitations of the Prior Approach

Case 1



Case 2



Case	Old Model	Expected Result
1	L1 greater than L2	L1 less than L2
2	L1 equal L2	L1 greater than L2

The Laplacian matrix can yield good approximation however it fails to compare and contrast between layout cases with these characteristics.



Mutual Inductance Impact Case Study

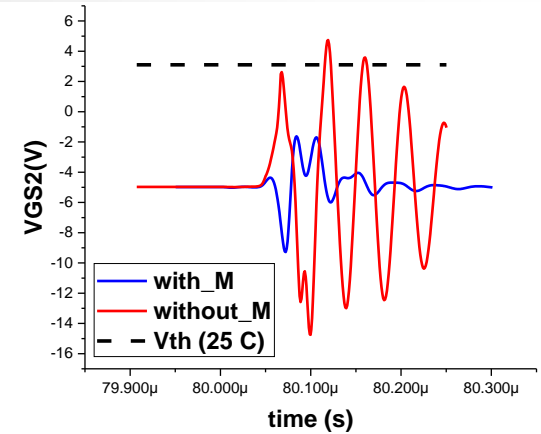
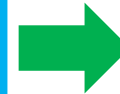
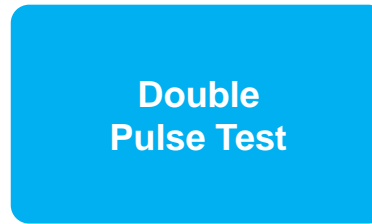
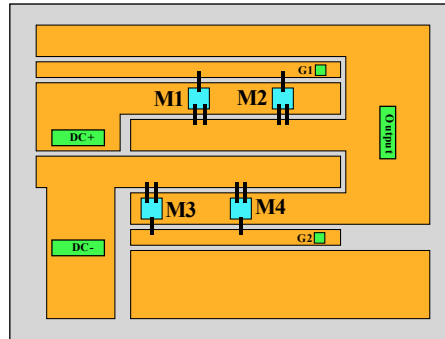
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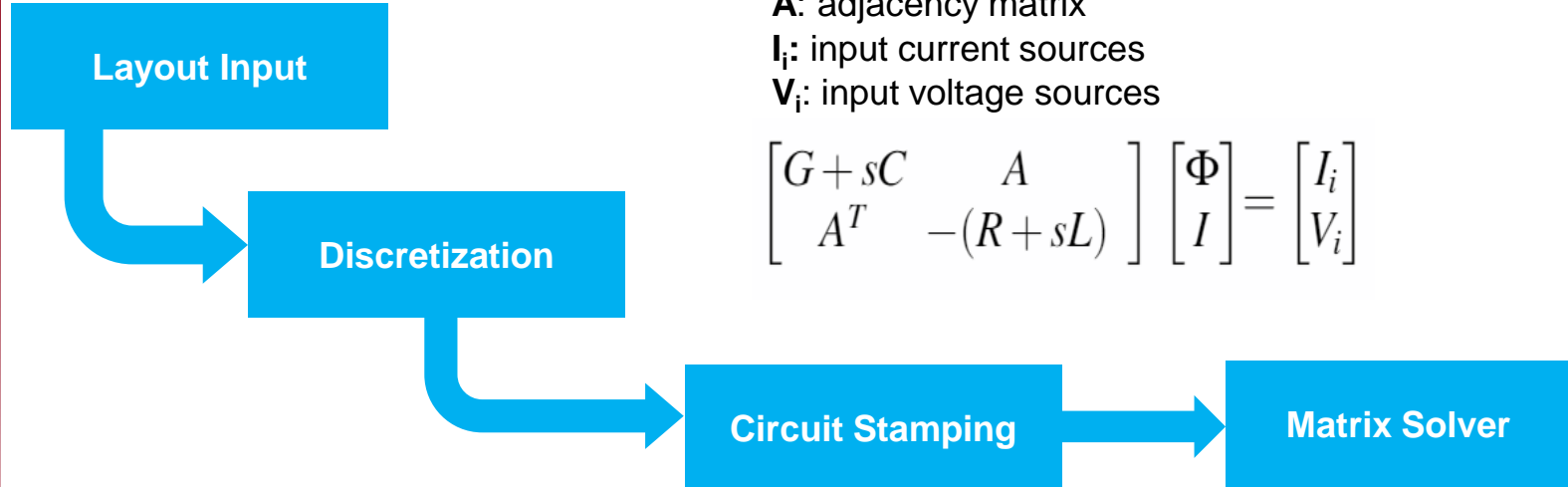
Conclusion



- Analyze gate signal integrity with and without mutual inductance impact.
 - False turn-on voltage in the gate-source signals has been observed in the two cases
 - More mutual impact with 3D layout cases
- Crucial to layout automation design
- We can consider most of these issues using PEEC techniques



PEEC Overview



The **P**artial **E**lement **E**quivalent **C**ircuit (PEEC) is a parasitics extraction technique using element stamping and matrix solving.



PEEC Overview

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Solution types:

No Current Solution:

$$[(\mathbf{G} + s\mathbf{C}) + \mathbf{A}(\mathbf{R} + s\mathbf{L})\mathbf{A}^T]\Phi = \mathbf{I}_i + \mathbf{A}(\mathbf{R} + s\mathbf{L})^{-1}\mathbf{V}_i]$$

No Voltage Solution:

$$[(\mathbf{R} + s\mathbf{L}) + \mathbf{A}^T(\mathbf{G} + s\mathbf{C})^{-1}\mathbf{A}]\mathbf{I} = -\mathbf{V}_i + \mathbf{A}^T(\mathbf{G} + s\mathbf{C})^{-1}\mathbf{I}_i]$$

Advantage:

- Can switch between above matrices formations to optimize evaluation time
- Current solution can be used to evaluate electric field and current density inside conductor
- Voltage solution can be used to evaluate electric field between different conductor

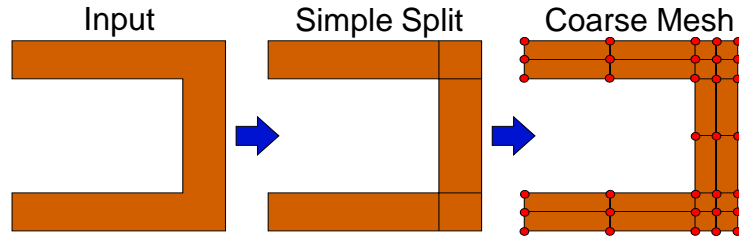
Disadvantage:

- Increased in computation time due to problem size in MCPM versus the skin-depth

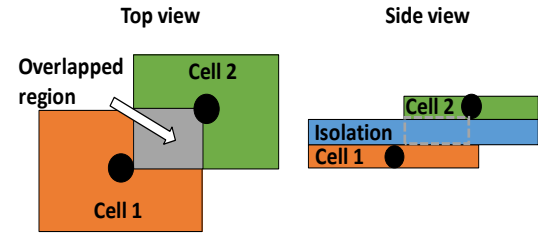
Meshing Process



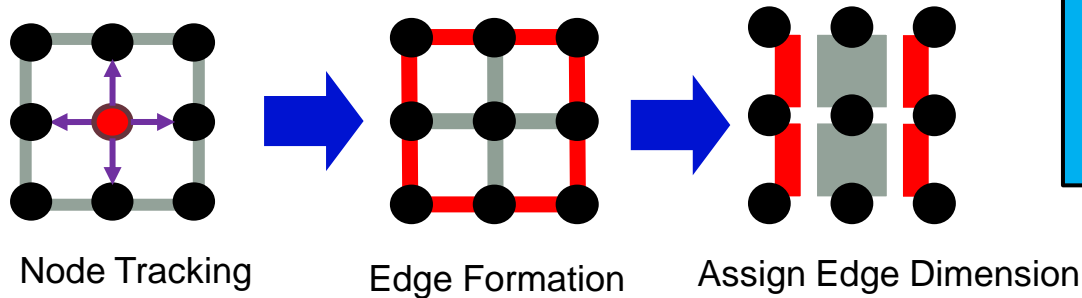
Coarse meshing:



Mesh for parasitic capacitance:



Edges and nodes assignment for R, L evaluation:



“A coarse mesh is used in this paper for branch current and node voltage evaluation with less computational effort”



RLCM Elements Evaluation

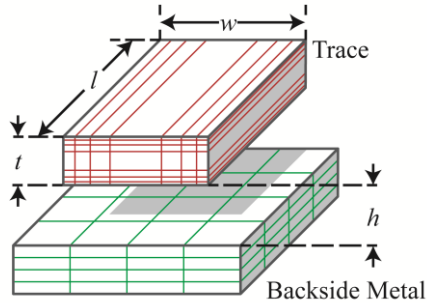
Overview

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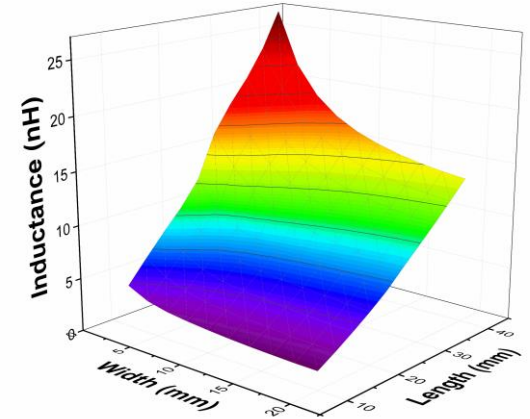
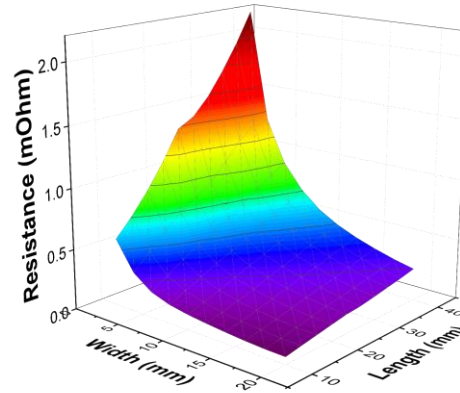
Methodology

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Meshing structure for response surface



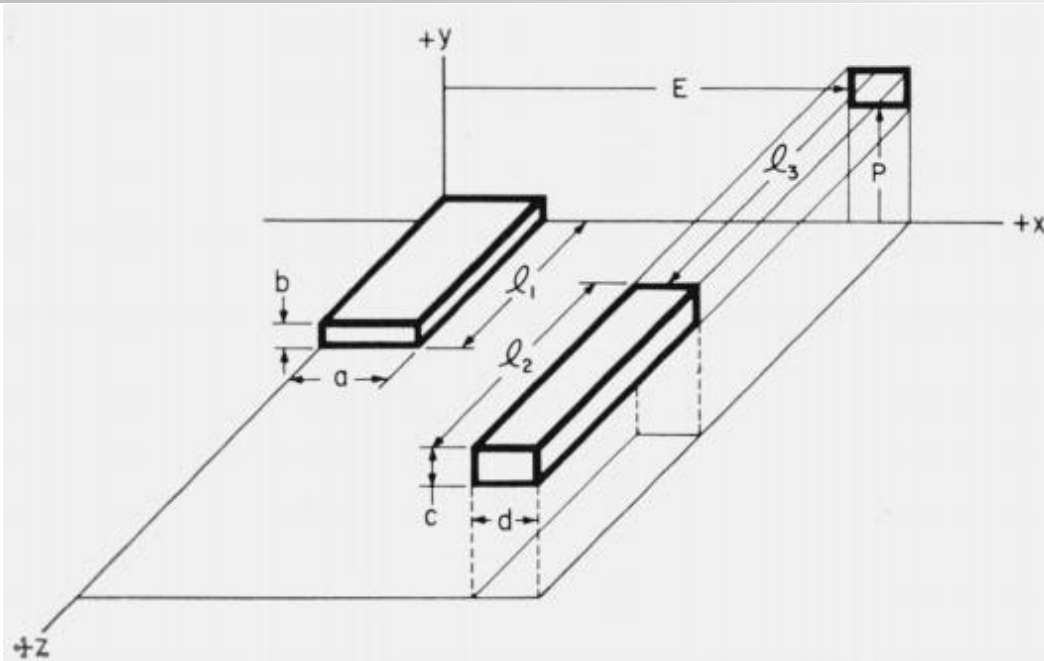
Trace resistance and inductance response surface

Pre-computed model through response surface technique [*]. These models take input width (W), length (L) of traces and frequency (f).

* Q. Le, T. Evans, S. Mukherjee, Y. Peng, T. Vrotsos and H. A. Mantooh, "Response surface modeling for parasitic extraction for multi-objective optimization of multi-chip power modules (MCPMs)," *2017 IEEE 5th Workshop on Wide Bandgap Power Devices and Applications (WIPDA)*, Albuquerque, NM, 2017, pp. 327-334.



RLCM Elements Evaluation

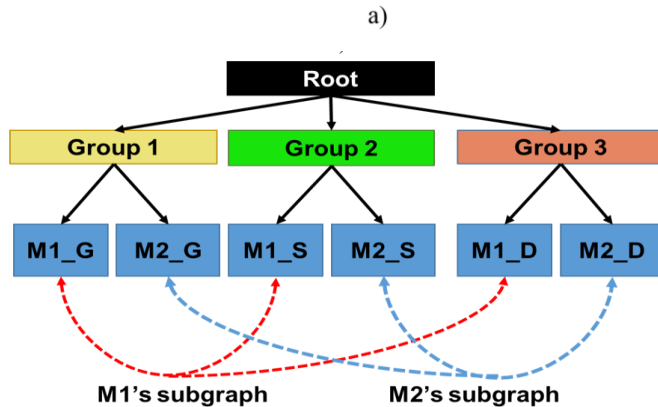
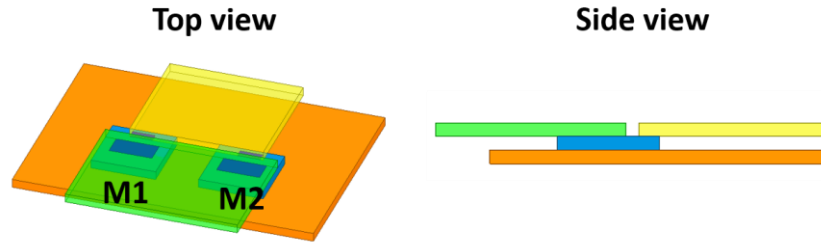


Exact analytical equation for mutual inductance calculation is used.

Take into account widths, lengths and distances between rectangular bars



Hierarchical Representation



Hierarchical representation:

- Symmetrical designs on same substrate.
- Reduces evaluation time.
- Meshing operation is independent for each group.

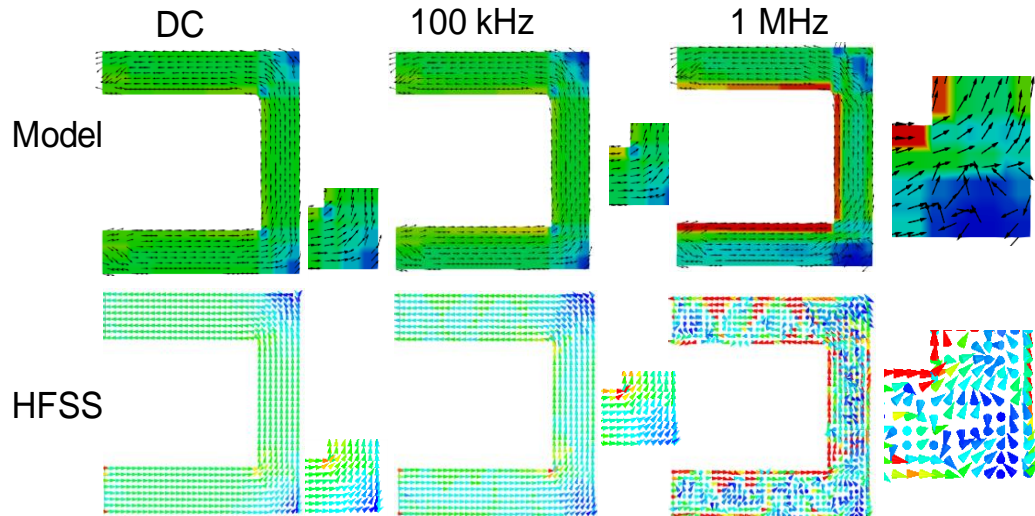
Components and terminals connections:

- Connections for devices and terminals in each different trace group are represented by a hierarchical tree structure.
- A subgraph is used to represent components internal parasitics (if they exist).



Current Density Extraction Results

Simple 10 mm x 10 mm U-shaped structure



Test case 1

Evaluation time comparison

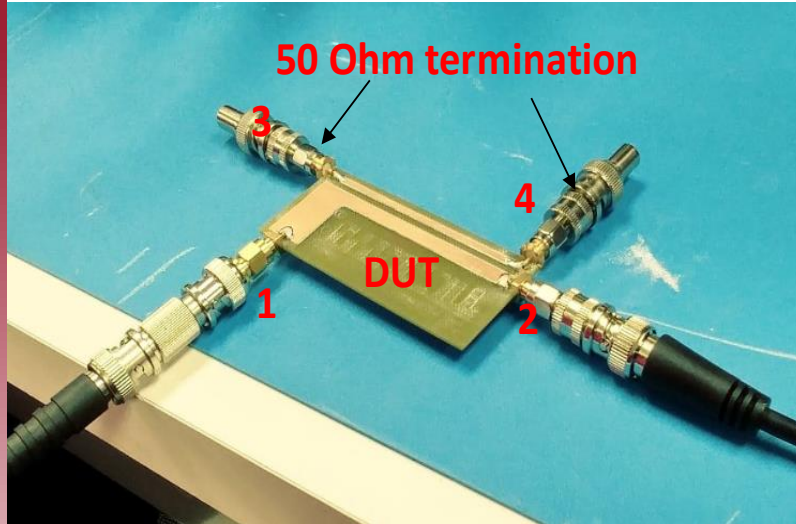
Method	Evaluation Time	#Mesh
Model	<u>30 ms</u>	120
HFSS	180 s	1371

- Current density results are extracted using model and compared with Ansys HFSS.
- Good agreement versus HFSS simulation

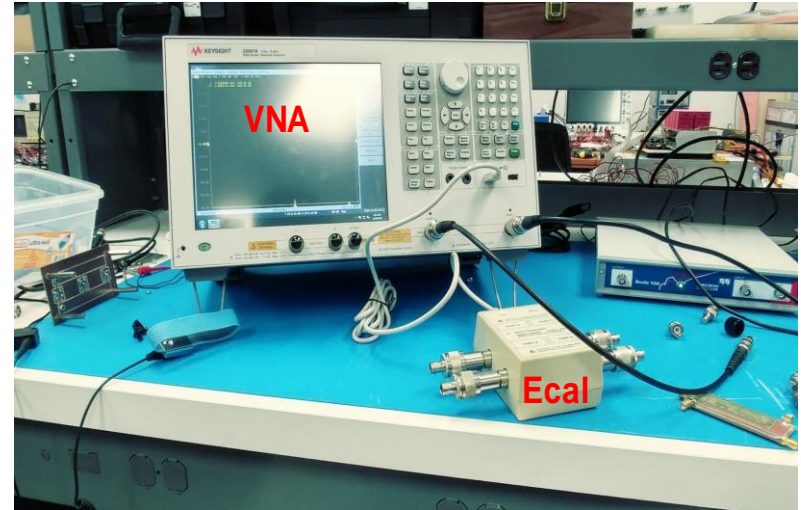


Experimental Setup for Coupling Verification

4-port test board



Experiment setup using Keysight E5061B VNA



- Netlist is extracted using model for each selected frequency from 10 kHz – 1 GHz
- Synopsys Hspice was used to extract the s-parameter from the netlist
- Same layout is simulated in ANSYS HFSS for validation

Test case 2



Experimental Results for Coupling Verification

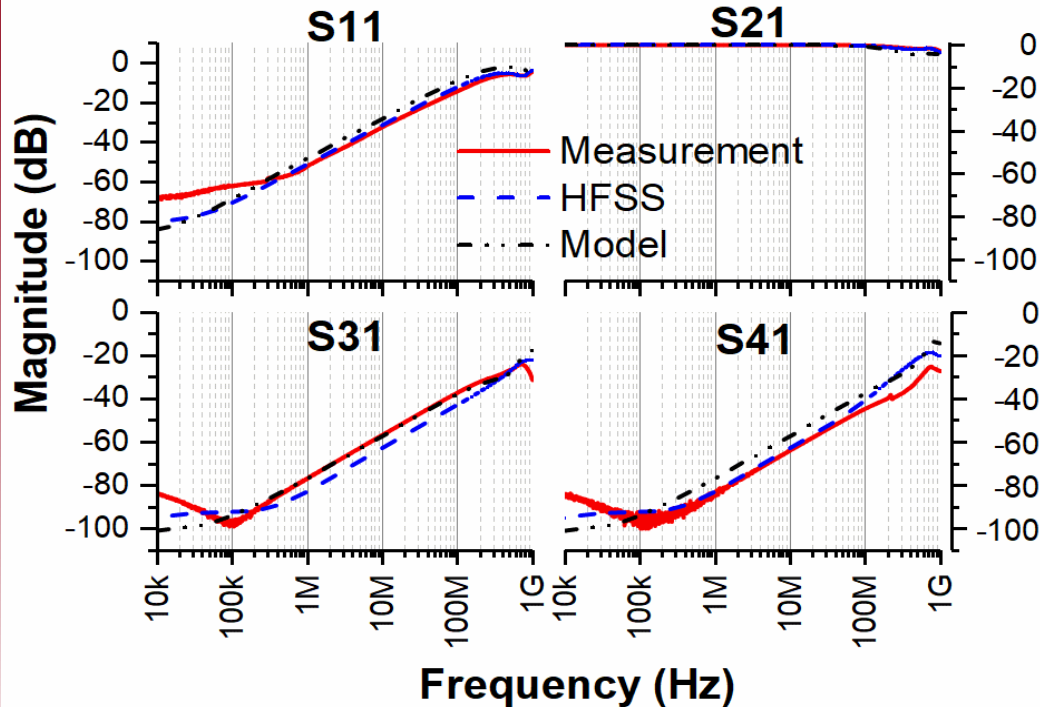
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- Measurement results show some noise in the frequency range less than 100 kHz.
 - Lower dynamic range at intermediate frequency of 3 kHz
 - Contact resistance between solder and SMA connector
- Results fit very well in the high-frequency region (>100 kHz).



Current Density Extraction @ 1MHz

Overview

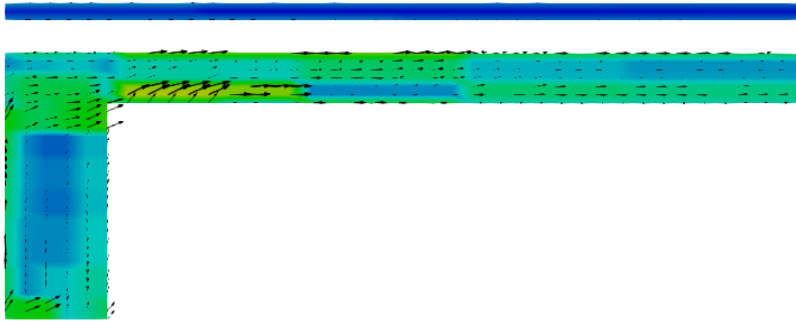
Motivation

Methodology

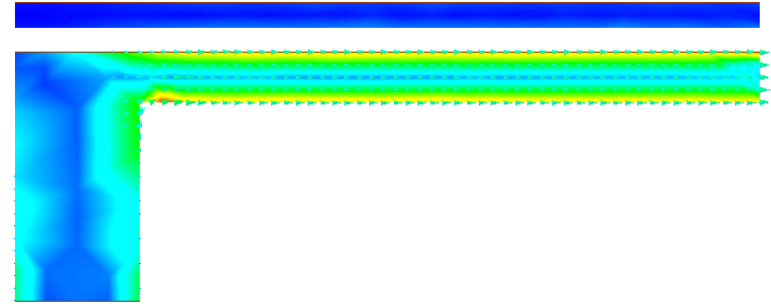
Results

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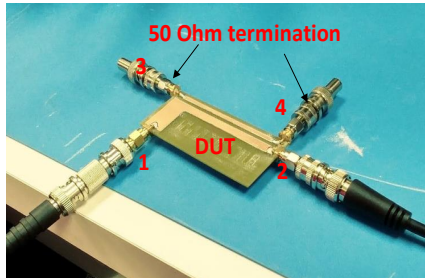
Model



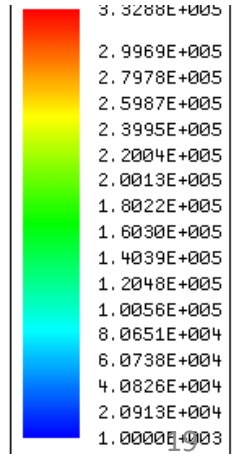
HFSS



Test Structure



Good current density agreement
with HFSS

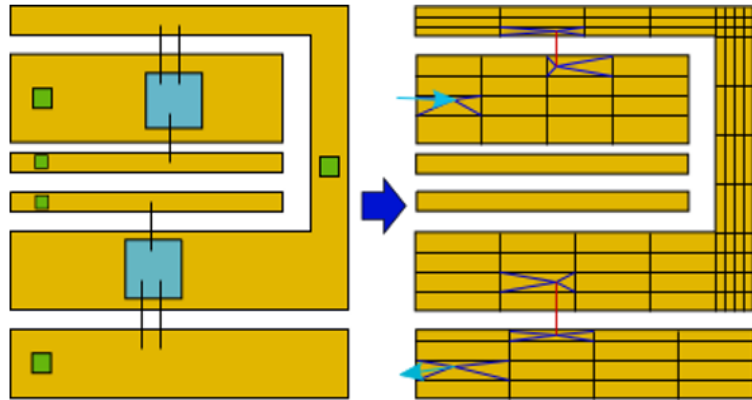




Experimental Result for Loop Verification

- Overview
- Motivation
- Methodology
- Results
- Conclusion

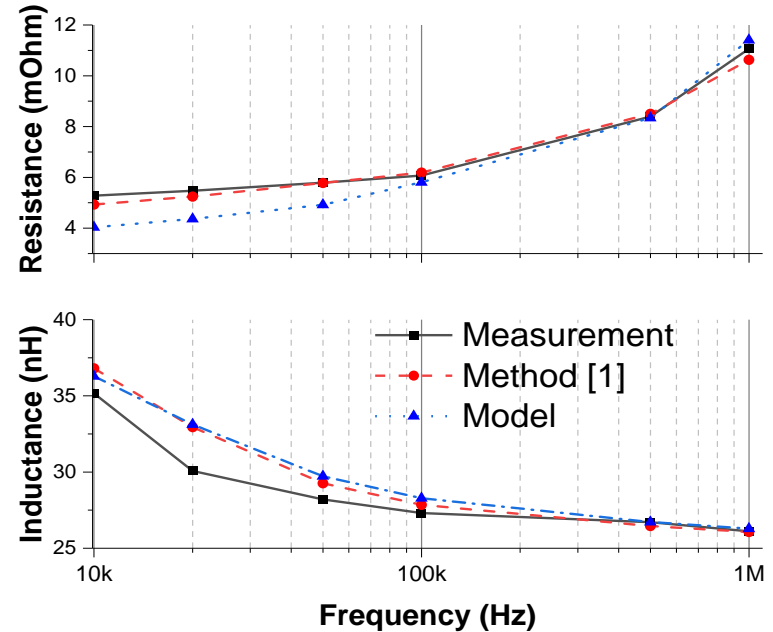
Layout and Mesh Structure



— Mesh edge
— Hierarchical edge
— Bondwire edge

Test case 3

Parasitics Extraction and Measurement Comparison



[1] T. M. Evans *et al.*, "PowerSynth: A Power Module Layout Generation Tool," in *IEEE Transactions on Power Electronics*.



Extraction Time Comparison

Overview

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Methodology

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	FastHenry	Previous Model [1]	Model without M	Model with M
Extraction Time	~300 s	~50 ms	~180 ms	~1.5 s
Speed-up Factor	1	x6000	x1666	x200
Mutual Inductance	Yes	No	No	Yes
I/V Distribution	No	No	Yes	Yes

Conclusion and Future Work



- Accurate model considering mutual coupling and I,V information during optimization.
- Validation through S-parameter measurement.



- Validation for 3D layout.
- Combine with layout engine and optimization engine for layout optimization.
- EMI mitigation model



References

- [1] Bindra and A. Mantooth, "Modern Tool Limitations in Design Automation: Advancing Automation in Design Tools is Gathering Momentum," in *IEEE Power Electronics Magazine*, vol. 6, no. 1, pp. 28-33, March 2019.
- [2] T. M. Evans *et al.*, "PowerSynth: A Power Module Layout Generation Tool," in *IEEE Transactions on Power Electronics*.
- [3] Q. Le, T. Evans, S. Mukherjee, Y. Peng, T. Vrotsos and H. A. Mantooth, "Response surface modeling for parasitic extraction for multi-objective optimization of multi-chip power modules (MCPMs)," *2017 IEEE 5th Workshop on Wide Bandgap Power Devices and Applications (WiPDA)*, Albuquerque, NM, 2017, pp. 327-334.
- [4] C. Hoer and C. Love, "Exact Inductance Equations for Rectangular Conductors with Applications to more Complicated Geometries," *J. Res. Natl. Bur. Stand. Sect. C Eng. Instrum.*, vol. 69C, p. 127, 1965



Acknowledgement





Thank you for your attention !

Merci de votre attention!